

# Effect of soft segment length on the properties of polyurethane anionomer dispersion

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(Received 6 August 1993)

Aqueous polyurethane anionomer dispersions were prepared from isophorone diisocyanate, poly(tetramethylene adipate glycol) (PTAd) and dimethylol propionic acid as potential anionic centres. The effects of polyol molecular weight ( $M_n$ ) on the state of dispersion, thermal, mechanical and viscoelastic properties and swelling of emulsion-cast film were determined. With increasing  $M_n$  of PTAd, the particle size of the emulsion and soft segment glass transition temperature,  $T_g$ , decreased, and solvent swelling, emulsion viscosity and hard segment  $T_g$  increased. Tensile strength showed a minimum with PTAd 1000, and elongation at break generally increased with the  $M_n$  of PTAd. These results could be interpreted in terms of soft segment-hard segment phase separation and crystallization of high molecular weight PTAd.

(Keywords: polyurethane; molecular weight; emulsion-cast film)

## Introduction

Polyurethane (PU) ionomers are segmented copolymers that consist of alternating soft and hard segment units, with a minority of repeat units carrying pendent acid or tertiary nitrogen groups which are neutralized to form salts. The soft segment generally consists of polyether or polyester polyol, whereas hard segments are usually formed by the extension of a diisocyanate with a chain extender of a low molecular weight polyol or amine.

It is now generally accepted that the properties of PU ionomers are primarily due to the phase behaviour of soft and hard segments as well as ion character. The existence of the hard segment domain, in particular, may give PU ionomer its excellent mechanical strength<sup>1,2</sup>. An elevation in the soft segment glass transition temperature ( $T_g$ ) is observed mainly as a result of the presence of dissolved hard segment<sup>3,4</sup>. In general, the polyester soft segment was found to contribute to phase mixing by hydrogen bonding between the oxygen of the soft segment and NH groups of the hard segment<sup>5,6</sup>. This behaviour also depends on the content, length and polarity of soft and hard segment. Many previous investigations<sup>7-11</sup> have reported on the characterization of this micro-domain structure in segmented PU. However, with regard to PU aqueous dispersion, most work was done by industrial laboratories, and basic structure/property behaviour is sparse in the open literature<sup>12-14</sup>.

In this paper we describe the preparation and properties of PU ionomer dispersions from poly(tetramethylene adipate glycol) (PTAd), isophorone diisocyanate (IPDI) and dimethylol propionic acid (DMPA). The effects of soft segment molecular weight ( $M_n = 600-2000$ ) on the emulsion characteristics and properties of emulsion-cast films are studied.

## Experimental

**Materials.** PTAd (Dongsung Chemicals) was dried and degassed at 80°C, 1-2 mmHg, for 5 h before use.

DMPA (Aldrich) was dried at 100°C for 2 h in a drying oven. Extra-pure grades of IPDI (Huls Chemicals) and dibutyltin dilaurate (DBT) were used as received. Dimethylformamide (DMF), triethylene tetramine (TETA), triethylamine (TEA), and solvents used in titration were dried over 3 Å molecular sieves before use.

**Prepolymer synthesis.** The basic formulation is given in Table 1. A 500 ml round-bottom, four-necked separable flask with a mechanical stirrer, thermometer, condenser with drying tube and a pipette outlet was used as reactor. Reaction was carried out in a constant-temperature oil bath. PTAd, DBT (0.03 wt% based on the total solid weight), and DMPA dissolved in DMF (5 wt% based on the total weight) were charged into the dried flask. While stirring, the mixture was heated to 90°C for about 30 min, followed by adding IPDI to the homogenized mixtures. The mixture was heated to 90°C for about 3 h to obtain NCO-terminated prepolymers. The change of NCO value during the reaction was determined using a standard dibutylamine back-titration method<sup>15</sup>. Upon obtaining the theoretical NCO value, the prepolymers were cooled to 60°C, and the neutralizing solution, i.e. TEA dissolved in DMF (5 wt% based on the total weight), was added and stirred for 1 h while maintaining the temperature at 60°C. The 1:1 stoichiometry was obtained by adding TETA at the chain extension step. The amount of DMF used in each step, i.e. to dissolve the DMPA and to reduce the solution viscosity, was approximately the same (see the total amount in the tables).

**Emulsification and chain extension.** Aqueous dispersion of PU was obtained by adding water (35°C) to the mixture (60°C). Since the water addition rate, in addition to the viscosity ratio between prepolymer solution and water, is a critical parameter in obtaining stable dispersion, a tubing pump was used, and water was added for 6 min at a constant flow rate. The phenomena of phase inversion, viscosity and conductivity change during the emulsification process are well documented<sup>16-18</sup>. TETA

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dissolved in water was then fed to the emulsion for a period of 40 min, and chain extension was carried out for the next 2 h. The resulting product was a stable (over 6 months at room temperature) urea-urethane dispersion with a solids content of about 35%.

**Tests.** Particle size and distribution were measured with an Autosizer (Malvern IIC), and the state of dispersion was investigated by transmission electron microscopy (TEM, Hitachi H300). To obtain the micrographs, samples were stained with OsO<sub>4</sub> for 1 week. Tensile properties of the emulsion-cast films were measured using an Instron Tensile Tester at a crosshead speed of 100 mm min<sup>-1</sup> and an average of at least five measurements was taken. Films were prepared by casting the emulsion onto a Teflon plate, followed by drying at 80°C for 5 h. The resulting films were then heated overnight in an oven at 60°C under 2–3 mmHg. Microtensile test specimens were prepared according to ASTM D-1822. Dynamic mechanical tests were performed with a dynamic mechanical thermal analyser (d.m.t.a., Polymer Lab.) from -100°C to 100°C at a frequency of 1 Hz. To measure the swelling in water and dimethylformamide (DMF), films were immersed in solvent for 24 h at room temperature and the percentage swelling was determined by measuring the weight increase:

$$\% \text{ swelling} = \frac{w - w_0}{w_0} \times 100$$

where  $w_0$  is the weight of dried film and  $w$  is the weight of film at equilibrium swelling.

### Results and discussion

**Particle size and emulsion viscosity.** Throughout the experiments, the average molecular weight of NCO-terminated prepolymer was fixed at 4500. As the  $M_n$  of PTAd increases from 600 to 2000, the hard segment content decreases from 48 to 38%. Table 2 shows that the particle size decreases linearly with increasing  $M_n$  of PTAd. The Autosizer result was visually confirmed from TEM (Figure 1). In PU dispersion, the average particle size is governed mainly by the hydrophilicity of the

PU<sup>16–18</sup>. However, the hydrophilicity increases marginally with increasing  $M_n$  of PTAd in the present system (to be shown later). The decrease of particle size with increasing  $M_n$  of PTAd has to be related to the increased chain flexibility of PU.

The effects of chain flexibility on the particle size reduction should be at least two-fold. First, flexible particles are more deformable in shear field<sup>19,20</sup>. During phase inversion, the dispersed phases are broken many times into smaller ones. Second, chain flexibility reduces the solution viscosity, which directly contributes to the fine break-up of the dispersed phase. Assuming stress continuity at the interface, smaller dispersed-phase viscosity leads to greater dispersed-phase deformation according to<sup>21</sup>:

$$\eta_c \gamma_c = \eta_d \gamma_d$$

where  $\eta$  and  $\gamma$  are viscosity and rate of shear, and the subscripts c and d designate continuous and dispersed phase, respectively. These two contribute to the fine break-up of PU ionomer phase in water, leading to a smaller particle size. Conversely, when the particle-size decrease is mainly caused by the increased hydrophilicity, an equilibrium particle size is generally obtained due to the increased swelling of water at high hydrophilicity.

It is widely accepted that the ionic groups are located predominantly on the surfaces of particles and the ionomer dispersions are stabilized by the formation of electrical double layers<sup>1,2</sup>. As the flexibility of PU chain increases with increasing soft segment content, the formation of micelle structure in water, having ionic sites on the surface, will be more plausible. This augments the thickness of electrical double layers due to the effective structuring of the micelles, leading to an increase in effective volume of the dispersed phase of the emulsion. The rate of water swelling also increases as the particle size decreases, due to the increased total surface area of the particles. In addition, at fixed total volume the effective hydrodynamic volume increases with decreasing particle size<sup>22</sup>. These all contribute to the increased effective hydrodynamic volume of the dispersed phase, and the effect should be more pronounced with increasing chain flexibility, leading to a dramatic rise in viscosity with high  $M_n$  of PTAd.

**Thermal analysis.** Figure 2 shows the d.s.c. thermograms of PUs containing PTAds with different  $M_n$  values. Generally, the shorter the segments, the more compatible the hard and soft segments<sup>23</sup>. Therefore soft segments prepared from PTAd of higher  $M_n$  are more likely to be phase separated with hard segments. With phase-separated morphology, PTAd can be crystallized. Our d.s.c. thermogram shows the melting peaks for PTAd

Table 1 Basic formulation of the feed<sup>a</sup>

$M_n$ of PTAd	PTAd (g)	DMPA (g)	IPDI (g)	TEA (ml)	TETA (g)
600	18.6	1.93	12.45	2.0	1.18
1000	20.8	1.93	10.09	2.0	1.18
1500	22.2	1.93	8.68	2.0	1.18
2000	22.9	1.93	7.91	2.0	1.18

<sup>a</sup> NMP, 300 ppm; H<sub>2</sub>O, 55 g; DMF, 10 ml

Table 2 Effect of  $M_n$  of PTAd on emulsion characteristics and film properties

$M_n$ of PTAd	Particle diameter ( $\mu\text{m}$ )	Emulsion viscosity (cPs, 20°C)	Hardness (Shore A)	Modulus <sup>a</sup> (kg cm <sup>-2</sup> )		Tensile strength (kg cm <sup>-2</sup> )	Elongation at break (%)	% Swelling (20°C)	
				200%	300%			Water	DMF
600	0.192	10.3	78.1	13.2	10.2	232	311	48	351
1000	0.126	10.8	79.0	20.1	11.3	203	321	57	612
1500	0.107	12.9	90.4	27.8	54.2	291	473	74	836
2000	0.048	42.0	92.2	9.3	7.8	325	582	92	1276

<sup>a</sup> At 200% and 300% elongation

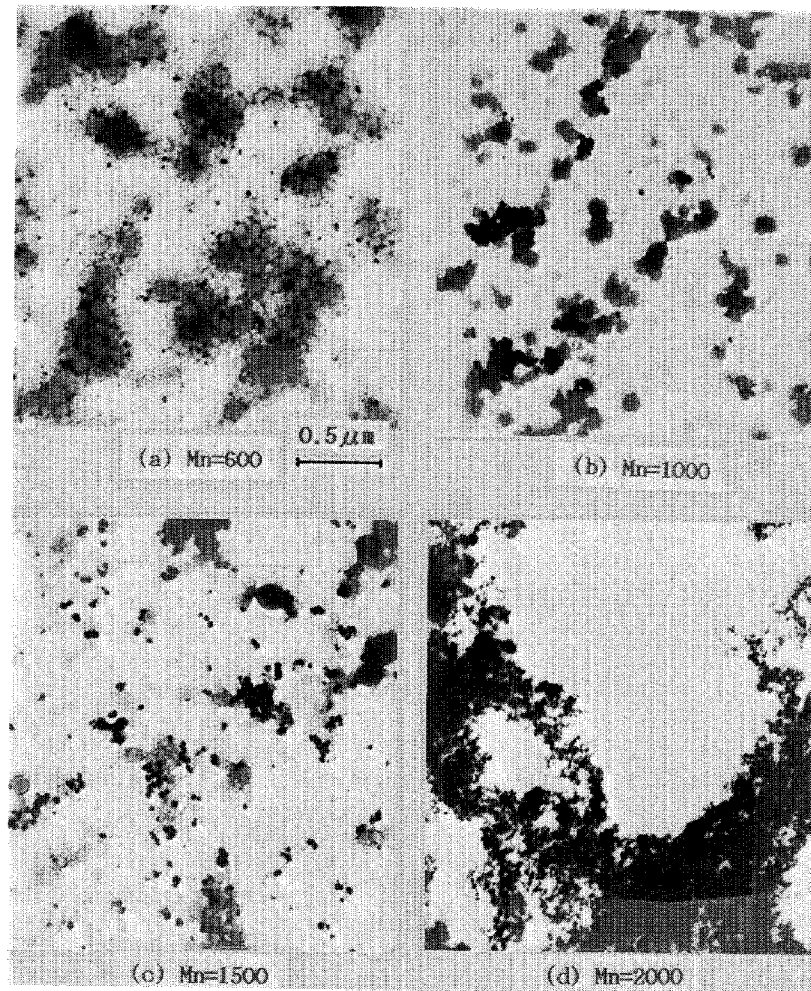


Figure 1 TEM micrographs for PU ionomer dispersions

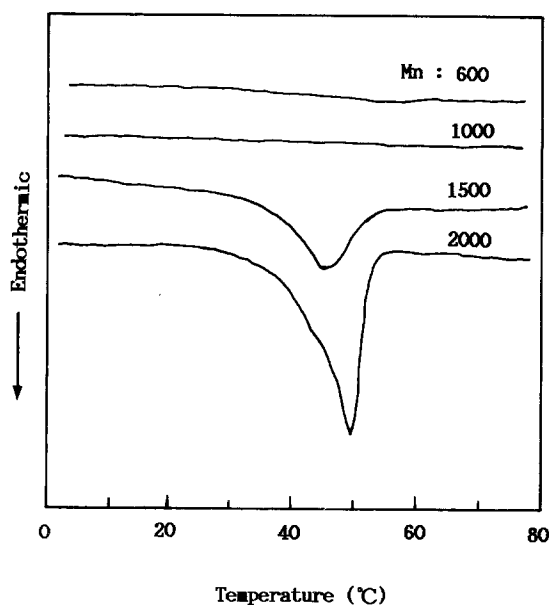


Figure 2 D.s.c. thermograms of the emulsion-cast films

1500 and 2000. Among these two, soft segment crystallization is more perfect and the crystalline melting temperature is higher for PTAd 2000 than for PTAd 1500. The increase of the melting point is attributed to an increase in the size of the crystallites or an increase

of complete crystalline phase due to the greater phase separation between the hard and soft segments.

*Viscoelastic properties.* The dynamic mechanical properties of the emulsion-cast films as a function of temperature are shown in Figure 3. The storage moduli ( $E'$ ) (Figure 3a) of PU from PTAd 600 and 1000 show similar behaviour to the thermoplastic, whereas those from PTAd 1500 and 2000 show an upturn at about 0°C. The upturn, leading to a higher value of  $E'$  at ambient temperature, should be related to the prevention of soft-hard phase mixing and soft segment crystallization<sup>24</sup>. When the phase mixing is relatively complete, the backbone mobility of soft segments is greatly restricted by the hard segments within the soft segments, and the hard segments are solubilized by the soft segments within the hard segments, and lose their effectiveness as a filler or a physical crosslink<sup>23</sup>. The loss modulus ( $E''$ ) peak (Figure 3b) at -25 to -35°C, corresponding to the  $T_g$  of the soft segment, is broader at lower  $M_n$  of PTAd, especially at PTAd 600, and it moves towards the lower temperature as the  $M_n$  of PTAd increases. The decrease of soft segment  $T_g$  with increasing  $M_n$  of PTAd is due to the increased degree of soft-hard phase separation. A broad shoulder in PTAd 600 is an indication of intimate phase mixing, and the overall effect would be to hinder the motion of soft segments and broaden the distribution of their relaxation times<sup>23</sup>. The peak at about -85°C can be attributed to the relaxation process involving the

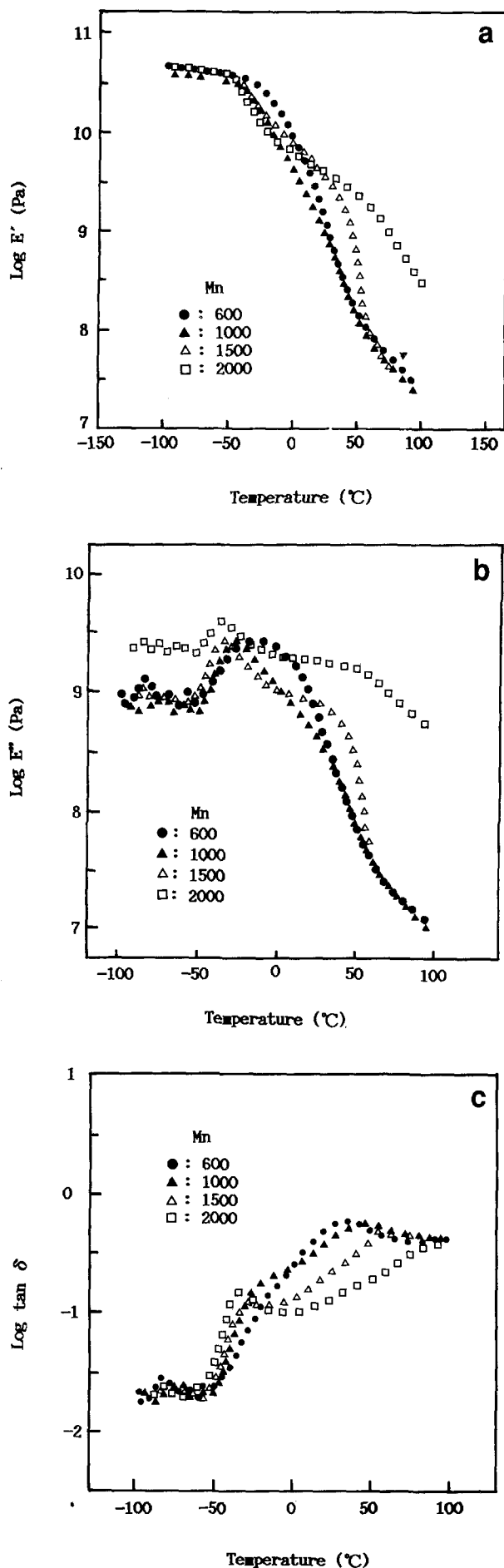


Figure 3 Dynamic mechanical properties of the emulsion-cast films: (a) storage modulus ( $E'$ ); (b) loss modulus ( $E''$ ); (c)  $\tan \delta$

local motion of methylene sequence of the polyester segment<sup>12,13</sup>.

The increased phase separation with increasing  $M_n$  of PTAd is again demonstrated in the  $\tan \delta$  curve (Figure 3c). With the increase of  $M_n$ , the lower peak (soft segment or soft-segment-rich phase  $T_g$ ) moves towards the lower temperature, and the higher peak (hard segment or hard-segment-rich phase  $T_g$ ) moves towards the higher temperature. The higher peak is defined for PTAd 600 and 1000 only, due to their relatively high hard segment content.

**Mechanical properties.** The tensile strength and elongation at break (Table 2) show that a minimum strength is obtained with PTAd 1000. The basic structure-property relationship in PU states that hard segments affect hardness and strength, and are controlled by the total NCO content<sup>25</sup>. As the  $M_n$  of PTAd increases, fewer hard segment and urethane linkages are formed, resulting in decreased strength for PTAd 1000. As the  $M_n$  of PTAd increases further, soft-hard phase separation becomes evident and soft segments crystallize. These two factors, i.e. phase separation and soft segment crystallization, contribute to the strength<sup>26</sup>. The increase of elongation with  $M_n$  of PTAd comes primarily from the augmented phase separations, which provide PU with more perfect physical networks than in the phase-mixed morphology<sup>23</sup>.

**Swelling in water and DMF.** With the increase of  $M_n$  of PTAd from 600 to 2000, swelling in DMF (Table 2) increases over five-fold, whereas in water it increases only slightly. The overall hydrophilicity of PU slightly increases with the soft segment content. It seems that DMF is preferentially dissolved in the soft domain. At low  $M_n$  ( $\leq 1000$ ), swelling is favoured by the amorphous nature of the soft segment, and is retarded by the hard domains dissolved in soft segments. At high  $M_n$ , swelling is augmented by phase separation and retarded by the crystallinity of the soft domain; it seems that the former dominates.

#### References

- Lorenz, O., Haulena, F. and Klebon, O. *Angew. Makromol. Chem.* 1973, **33**, 159
- Lorenz, O. and Hick, H. *Angew. Makromol. Chem.* 1978, **72**, 115
- Sung, C. S. P., Smith, T. W. and Sung, N. H. *Macromolecules* 1980, **13**, 117
- Wang, C. B. and Cooper, S. L. *Macromolecules* 1983, **16**, 775
- Srichatrapimuk, V. O. W. and Cooper, S. L. *J. Macromol. Sci.-Phys.* 1974, **9**, 447
- Senich, G. A. and MacNight, W. J. *Macromolecules* 1980, **13**, 106
- Seefeld, C. G. Jr, Koleske, J. V. and Critchfield, F. E. *J. Appl. Polym. Sci.* 1975, **19**, 2493
- Al-Salah, H. A., Xiao, H. X., McLean, J. A. and Frisch, K. C. *J. Polym. Sci., Part A: Polym. Chem.* 1988, **26**, 1609
- Van Bogart, J. W. C., Liaonitkul, A., Lerner, L. E. and Cooper, S. L. *J. Macromol. Sci.-Phys.* 1980, **17**, 267
- Smith, T. L. *J. Polym. Sci., Polym. Phys. Edn.* 1974, **2**, 1825
- Wilkes, G. L. and Wildnauer, R. *J. Appl. Phys.* 1975, **46**, 4148
- Hwang, K. K. S., Speckhard, T. A. and Cooper, S. L. *J. Macromol. Sci.-Phys.* 1984, **23**, 153
- Yang, C. Z., Hwang, K. K. S. and Cooper, S. L. *Macromol. Chem.* 1983, **184**, 651
- Hwang, K. K. S., Yang, C. Z. and Cooper, S. L. *Polym. Eng. Sci.* 1981, **21**, 1027
- David, D. J. and Staley, H. B., 'Analytical Chemistry of Polyurethanes', High Polymer Series, XVI, Part III, Wiley-Interscience, New York, 1969
- Dieterich, D. *Prog. Org. Coatings* 1981, **9**, 281
- Kim, C. K., Kim, B. K. and Jeong, H. M. *Colloid Polym. Sci.* 1991, **269**, 895

- 18 Kim, T. K. and Kim, B. K. *Colloid Polym. Sci.* 1991, **269**, 889
- 19 Han, C. D. 'Multiphase Flow in Polymer Processing', Academic Press, New York, 1981
- 20 Utraki, L. A. 'Polymer Alloys and Blends', Hans Publishers, New York, 1989
- 21 Bird, R. B., Stewart, W. E. and Lightfoot, E. N. 'Transport Phenomena', Wiley, New York, 1960
- 22 Rutgers, I. R. *Rheol. Acta.* 1962, **2**, 305
- 23 Abouzahr, S. and Wilkes, G. L. *J. Appl. Polym. Sci.* 1984, **29**, 2695
- 24 Cooper, S. L. and Tobosky, A. V. *J. Appl. Polym. Sci.* 1966, **10**, 1837
- 25 Hepburn, C. 'Polyurethane Elastomer' 2nd Edn, Elsevier Applied Science, London, 1991
- 26 Petrovic, Z. R. *J. Polym. Sci., Part B: Polym. Phys.* 1989, **27**, 545